

1. Buck-Boost

(i)

$$V_d = V_{in} = 14V$$

$$V_o = 42V$$

$$P_o = 21W$$

$$\Delta i_L = 1,8A$$

$$f_s = 200kHz$$

$$V_o = \frac{D}{1-D} \cdot V_{in} \rightarrow \frac{V_o}{V_{in}} = \frac{D}{1-D} \rightarrow \frac{42}{14} = \frac{D}{1-D} \rightarrow D = 0,75$$

$$T_s = 1/f_s = 1/200 \cdot 10^3 = 5\mu s$$

$$t_{on} = D \cdot T_s = 0,75 \cdot 5\mu s = 3,75\mu s$$

$$P_o = V_o \cdot I_o \rightarrow I_o = \frac{P_o}{V_o} = \frac{21W}{42V} = 0,5A$$

$$I_{in} = \frac{D}{1-D} \cdot I_o = \frac{0,75}{1-0,75} \cdot 0,5A = 1,5A$$

$$I_L = I_{in} + I_o = 1,5 + 0,5 = 2A$$

$$\Delta i_L = \frac{V_{in} (D \cdot T_s)}{L} \quad \text{~~1,8 = \frac{14 (0,75 \cdot 5 \cdot 10^{-6})}{L}~~}$$

$$L = \frac{V_{in} (D \cdot T_s)}{\Delta i_L} = \frac{14 (0,75 \cdot 5 \cdot 10^{-6})}{1,8A} = 29,17\mu H$$

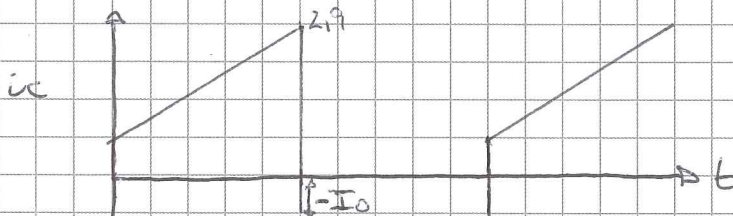
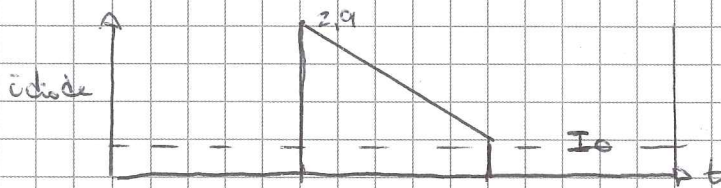
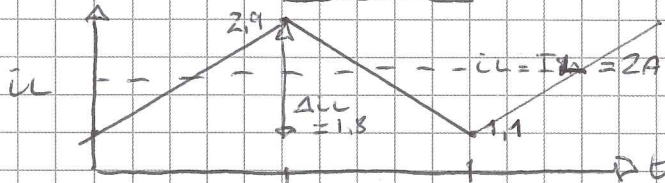
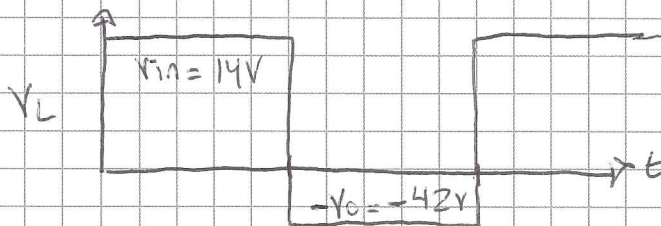
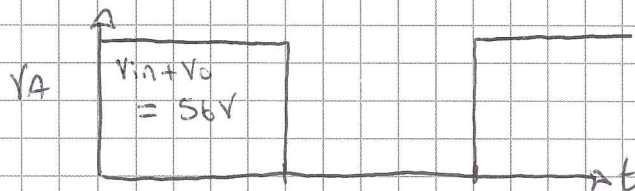
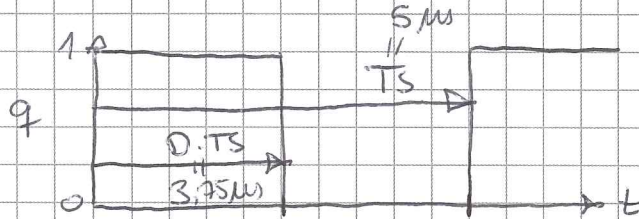
≈ 29,2 μH

$$i_{L, \max} = I_L + \frac{\Delta i_L}{2} = 2 + \frac{1,8}{2} = 2,9A$$

$$i_{L, \min} = I_L - \frac{\Delta i_L}{2} = 2 - \frac{1,8}{2} = 1,1A$$



1.
(i) continue.





1 (ii) Find $P_{o,crit}$

$$P_{o,crit} = V_o \cdot I_{o,crit}$$

$$\begin{cases} I_{L,crit} = \frac{1}{1-D} \cdot I_{o,crit} \\ I_{o,crit} = I_{L,crit} (1-D) \end{cases}$$

$$\Delta i_L = 1,8 \text{ A} = \overset{\wedge}{I_{L,crit}}$$

$$I_{L,crit} = 0,5 \cdot \overset{\wedge}{I_{L,crit}} = 0,5 \cdot 1,8 = 0,9 \text{ A}$$

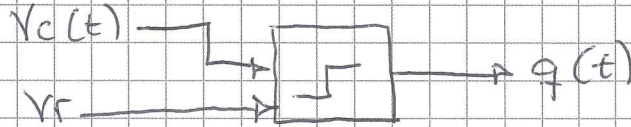
$$I_{o,crit} = 0,9 (1 - 0,75) = 0,225 \text{ A}$$

$$V_o = 42 \text{ V}$$

$$P_{o,crit} = V_o \cdot I_{o,crit}$$

$$= 42 \text{ V} \cdot 0,225 \text{ A} = 9,45 \approx \underline{\underline{9,5 \text{ W}}}$$

2.1

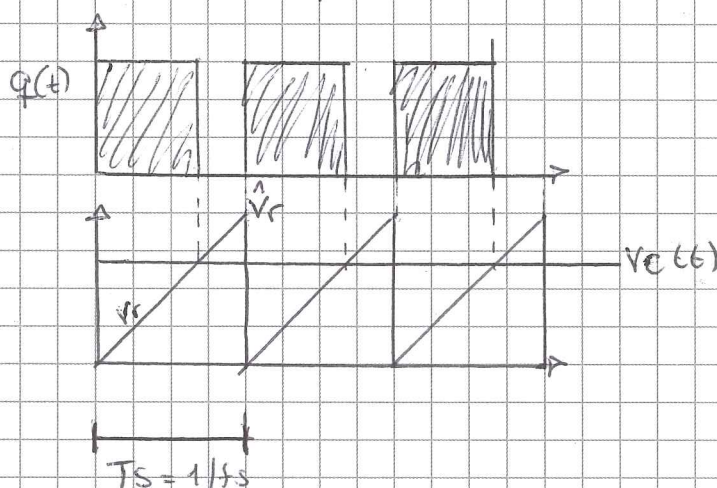


The output voltage V_o can be controlled by Pulse width modulating (PWM) the duty ratio $d(t)$.

V_o is compared to its reference value V_o^* , and the output is the control voltage $V_c(t)$. The control voltage is then compared with a ramp voltage V_r , making the output $q(t)$, which controls $d(t)$.

$q(t) = 1$ when $V_c(t)$ is greater than V_r , else 0.

$V_c(t)$ ranges between 0 and \hat{V}_r , which is the amplitude of V_r .

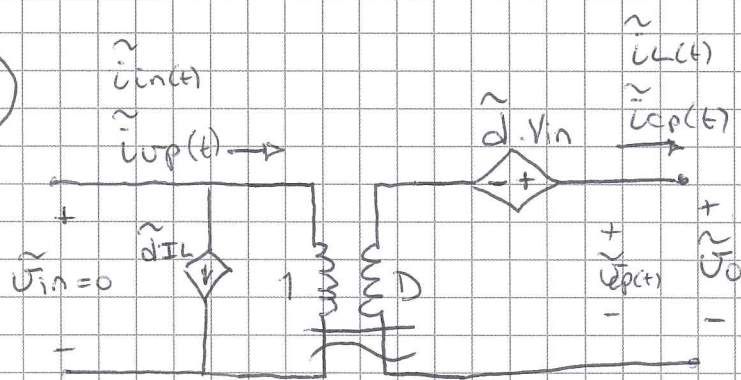


Linearized transfer-function of PWM:

$$G_{\text{PWM}}(s) = \frac{1}{\hat{V}_r} \frac{\tilde{d}(s)}{\tilde{V}_c(s)}$$



2.2



$$\begin{aligned}
 V_{cp} + \tilde{U}_{cp}(t) &= (D + \tilde{d}(t)) (V_{rp} + \tilde{U}_{rp}(t)) \\
 I_{vp} + \tilde{I}_{vp}(t) &= (D + \tilde{d}(t)) (I_{cp} + \tilde{I}_{cp}(t)) \\
 \tilde{U}_{cp}(t) &= (D \cdot \tilde{U}_{rp}(t)) + (\tilde{d}(t) \cdot V_{rp}) \\
 \tilde{I}_{vp}(t) &= (D \cdot \tilde{I}_{cp}(t)) + (\tilde{d}(t) \cdot I_{cp})
 \end{aligned}$$

3.1

$$V_s = 120V(\text{rms}) \quad I_{s1} = 10A(\text{rms})$$

$$P = 0,95 \text{ kW} \quad \text{THD} = 75\% \approx 0,75$$

a) $P = V_s \cdot I_{s1} \cdot \text{DPF}$

$$\begin{aligned}
 \hookrightarrow \text{DPF} &= \frac{P}{V_s \cdot I_{s1}} = \frac{0,95 \cdot 10^3}{\sqrt{2} \cdot 120 \cdot 10} = 0,5597 \approx 0,56 \\
 &\approx 56\%
 \end{aligned}$$

b) $\text{THD} = \frac{I_{\text{dist}}}{I_{s1}} \rightarrow I_{\text{dist}} = \text{THD} \cdot I_{s1}$

$$= 0,75 \cdot 10 = \underline{\underline{7,5A}}$$

c) $\text{PF} = \frac{I_{s1}}{I_s} \cdot \text{DPF} = \frac{10}{12,5} \cdot 0,56 = 0,448$

$$\approx \underline{\underline{0,45}}$$

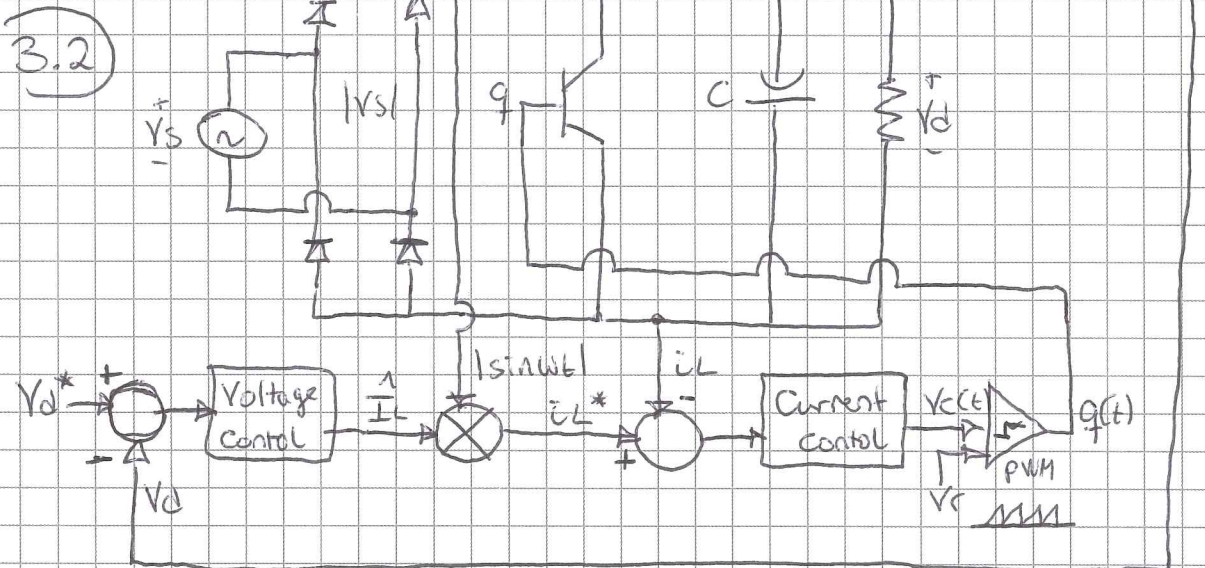
$$I_s^2 = I_{s1}^2 + I_{\text{dist}}^2$$

$$I_s = \sqrt{I_{s1}^2 + I_{\text{dist}}^2} = \sqrt{10^2 + 7,5^2} = 12,5A$$

Comments on next page →



3.1 c) Comments: The ~~fundamental~~ ^{distortion} component of I_s is 7.5A, which is 75% I_{s1} .
 The distortion makes I_s less sinusoidal (due to noise/harmonics) making the overall PF low, and the circuit delivers less power. A voltage and current control circuit as drawn below can help with this by PWM to PFC.



The main objective is to draw the current in phase with the voltage.

The voltage and current control loops are used to PWM the duty ratio $d(t)$ to control the output voltage V_d .

V_d is used in voltage control to estimate the amplitude of i_L (I_L^*), and $|sin\omega t|$ is used to estimate the form of i_L .



4.1) $P = \frac{1}{2} \cdot \hat{I}_s \cdot \hat{V}_s \rightarrow \hat{I}_s = \frac{P}{\sqrt{2} \cdot \hat{V}_s} = \frac{250W}{\sqrt{2} \cdot 120V} = 1,47$
 $\hat{I}_L = \hat{I}_s$

$i_L(t) = \hat{I}_L |\sin \omega t| = 1,47 |\sin \omega t|$

$d(t) = 1 - \frac{\hat{V}_s |\sin \omega t|}{V_d} = 1 - \frac{\sqrt{2} \cdot 120}{250} |\sin \omega t|$
 $= 1 - 0,68 |\sin \omega t|$

$\bar{i}_d(t) = \frac{1}{2} \cdot \frac{\hat{V}_s}{V_d} \cdot \hat{I}_L - \frac{1}{2} \frac{\hat{V}_s}{V_d} \cdot \hat{I}_L |\cos 2\omega t|$

$= \frac{1}{2} \cdot \frac{\sqrt{2} \cdot 120}{250} \cdot 1,47 - \frac{1}{2} \cdot \frac{\sqrt{2} \cdot 120}{250} \cdot 1 |\cos 2\omega t|$

$= \frac{0,5}{I_d} - 0,5 |\cos 2\omega t|$

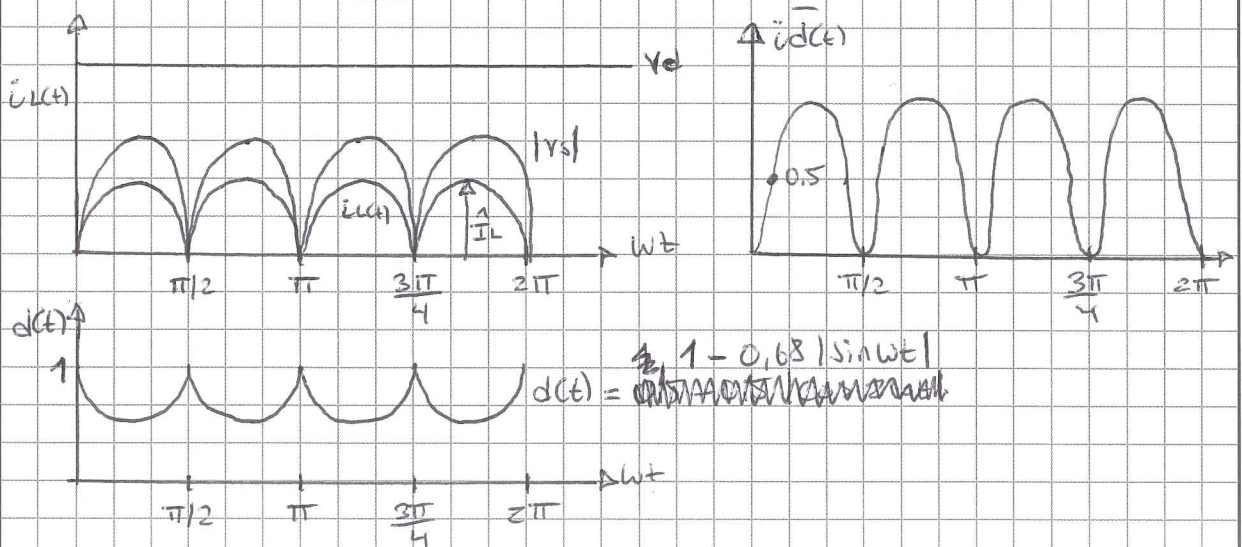
↑ $i_{d2}(t)$ second harmonic = current through the capacitor

$\omega_s = 2 \cdot \pi \cdot f_s = 2 \cdot \pi \cdot 100 \cdot 10^3$

$\bar{i}_c(t) = \left(\frac{1}{2\omega C} \right) \left(\frac{1}{2} \frac{\hat{V}_s}{V_d} \cdot \hat{I}_L \cdot |\cos 2\omega t| \right)$

$= \left(\frac{1}{4 \cdot 2 \cdot \pi \cdot 100 \cdot 10^3 \cdot 220 \cdot 10^{-6}} \right) \cdot \left(\frac{\sqrt{2} \cdot 120}{250} \cdot 1,47 \right) \cdot |\cos 2\omega t|$

$= 1,8 \cdot 10^{-3} |\cos 2\omega t|$





4.2) At full load :

$$P = 250\text{W} \quad \hat{V}_s = \sqrt{2} \cdot 120 \quad \hat{I}_s = 1,47$$

$$\text{So } i_c = 1,8 \cdot 10^{-3} |\cos 2\omega t|$$

$$i_c = C \cdot \frac{dV_c}{dt} \quad \text{and since } V_o = V_c$$

$$i_c = C \cdot \frac{dV_o}{dt} \quad \rightarrow \quad \frac{dV_o}{dt} = \frac{i_c}{C}$$

$$\Delta V_o = \frac{dV_o}{dt} = \frac{1,8 \cdot 10^{-3} \cdot |\cos 2\omega t|}{220 \cdot 10^{-6}} = \underline{\underline{8,18 \cdot |\cos 2\omega t|}}$$

$$\text{Boost: } V_o = \frac{1}{1-D} \cdot V_{in} \quad \rightarrow \quad V_{in} = V_o(1-D)$$

$$\Delta V_{in} = 8,18 |\cos 2\omega t| (1-0,32)$$

$$= \underline{\underline{5,6 \cdot |\cos 2\omega t|}}$$

$$\frac{V_o}{V_{in}} = \frac{1}{1-D}$$

$$\frac{250}{\sqrt{2} \cdot 120} = \frac{1}{1-D}$$

$$\rightarrow D = 0,32$$